

Vivien Chen (NTHU)

Aperture Synthesis and Interferometers

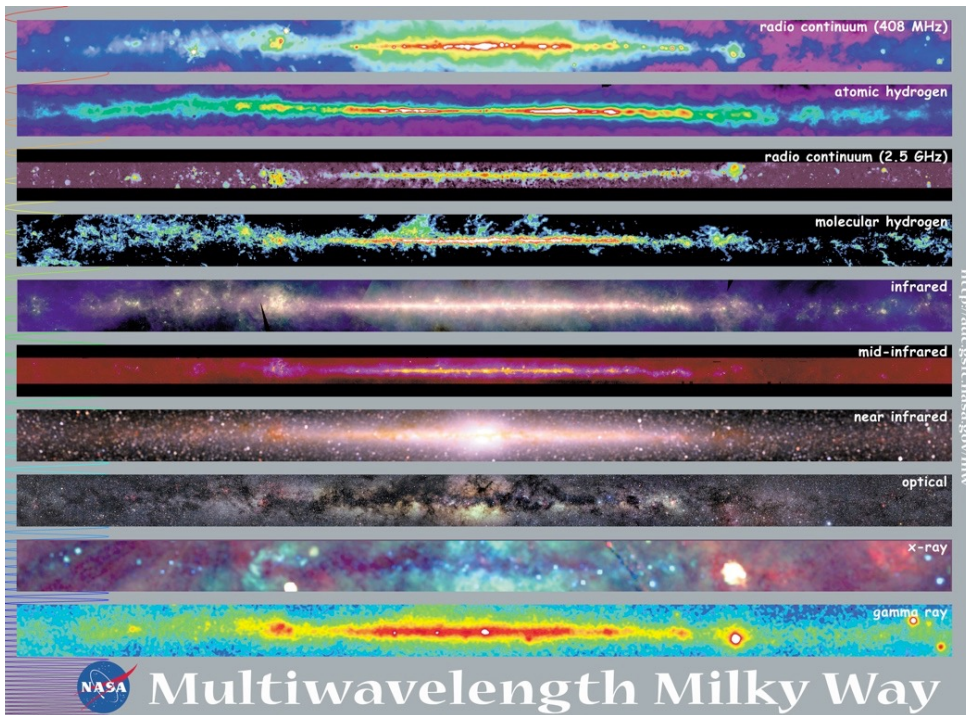
Recommended readings:

Clark 1999, ASPC, 180, 1; Thompson 1999, ASPC, 180, 11

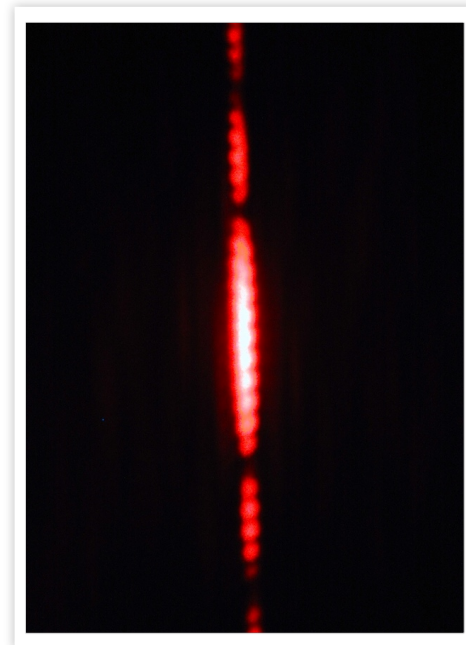
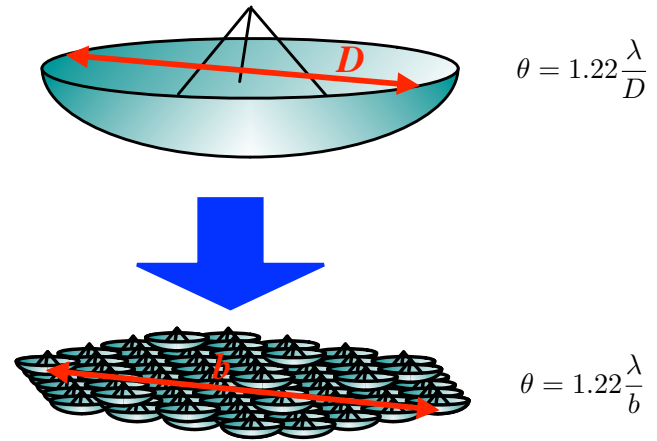
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Fundamentals of Radio Interferometry

Observation strategies



What are interferometers?



Introduction to Interferometry

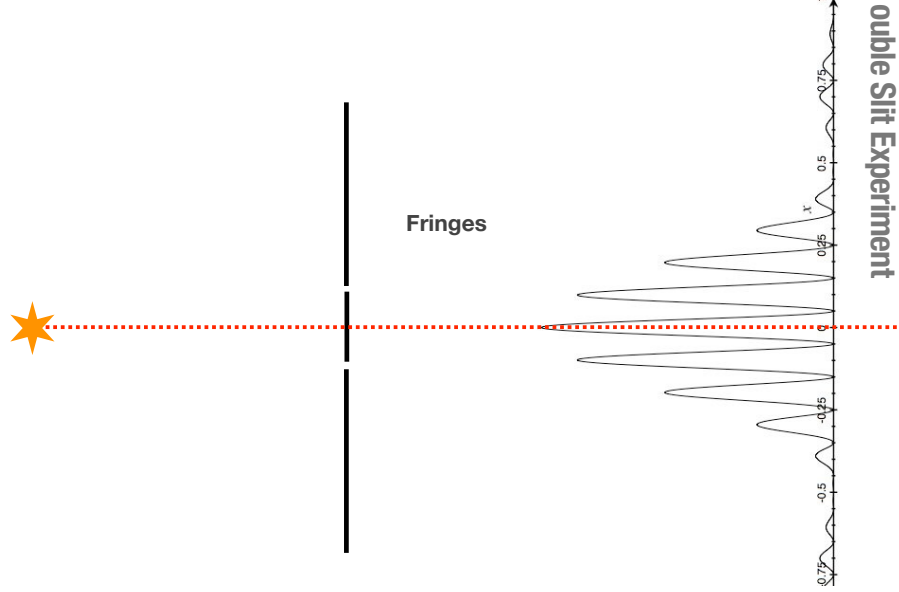
The double-slit experiment as an example

Double-slit Experiment

5

D

Double Slit Experiment

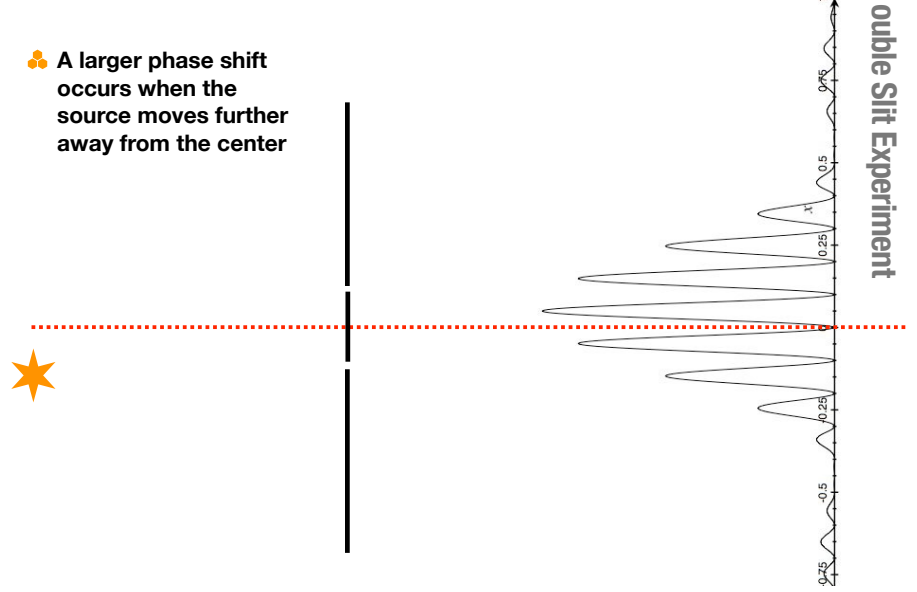


Double-slit Experiment

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Double Slit Experiment

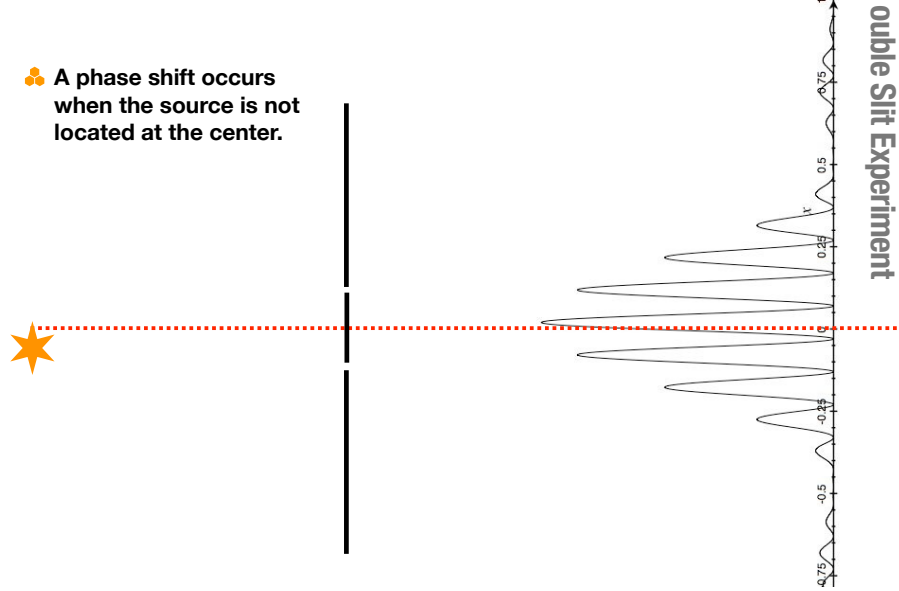


Double-slit Experiment

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Double Slit Experiment

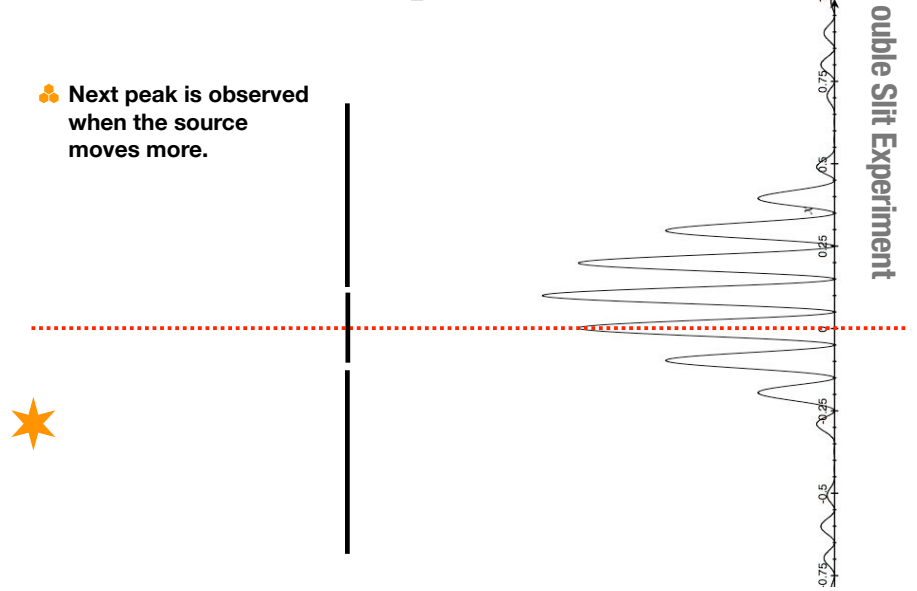


Double-slit Experiment

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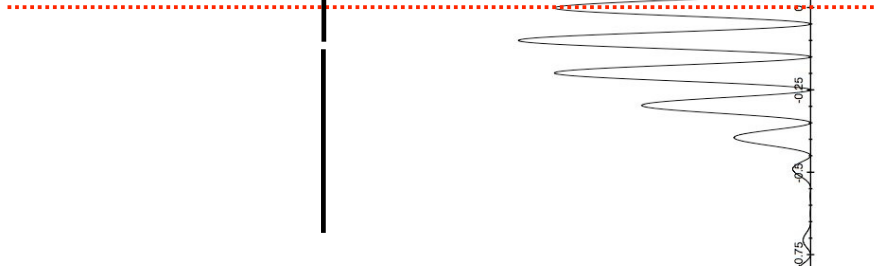
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Double Slit Experiment



Double-slit Experiment

- A similar phase shift is expected when the source moves in the opposite direction.

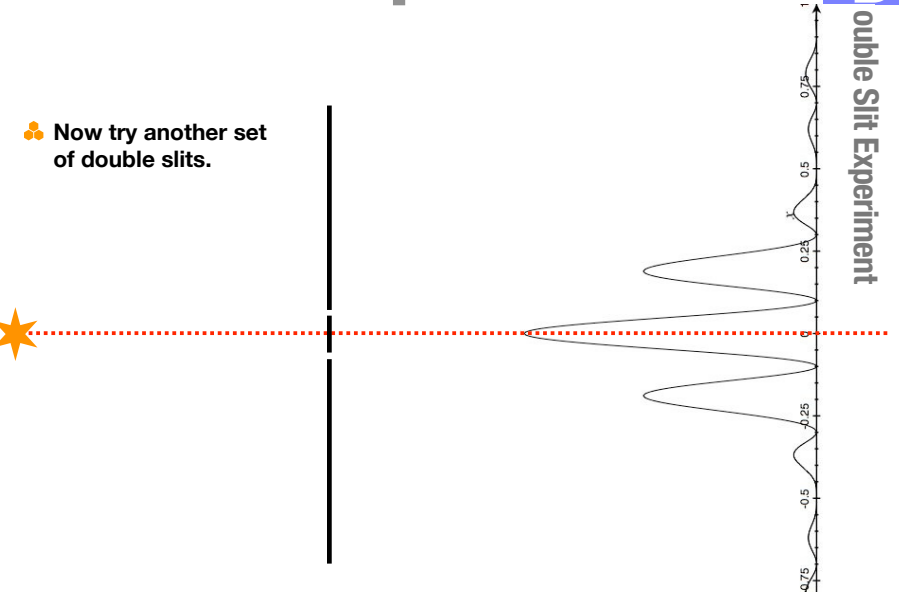


Double Slit Experiment

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Double-slit Experiment

- Now try another set of double slits.

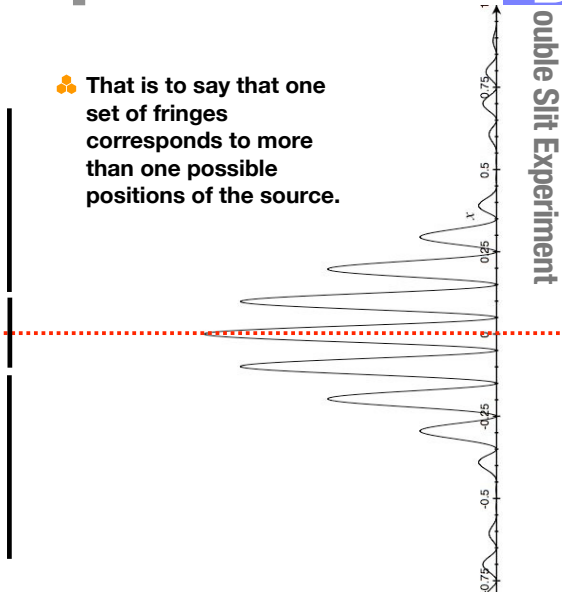


Double Slit Experiment

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Double-slit Experiment

- That is to say that one set of fringes corresponds to more than one possible positions of the source.

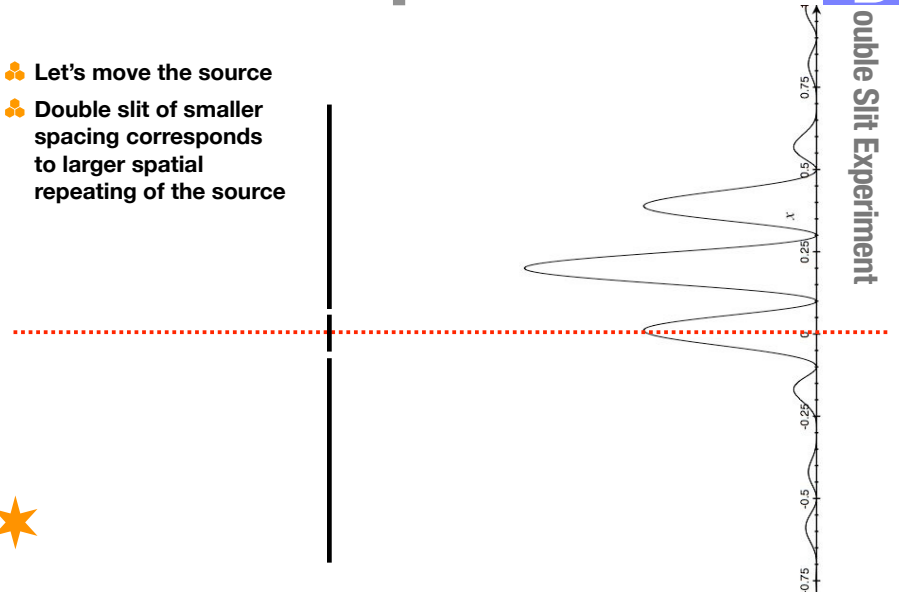


Double Slit Experiment

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Double-slit Experiment

- Let's move the source
- Double slit of smaller spacing corresponds to larger spatial repeating of the source



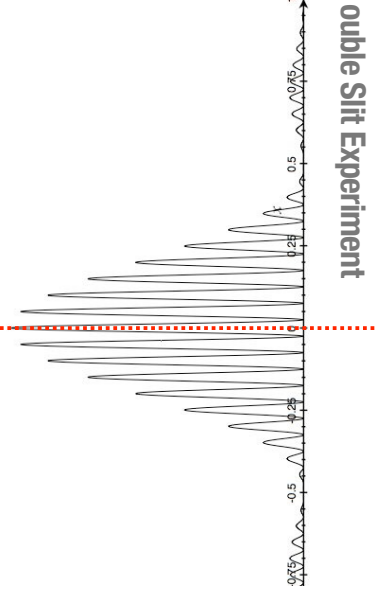
Double Slit Experiment

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Double-slit Experiment

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How about a double slit of larger spacing?

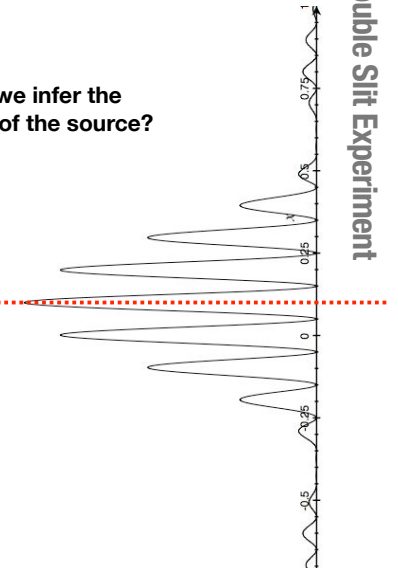


Double Slit Experiment

Double-slit Experiment

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How do we infer the position of the source?

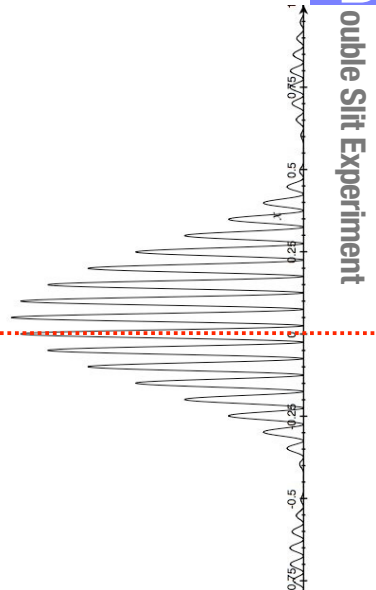


Double Slit Experiment

Double-slit Experiment

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Let's move the source
Double slit of larger spacing corresponds to smaller spatial repeating of the source



Double Slit Experiment

Double-slit Experiment

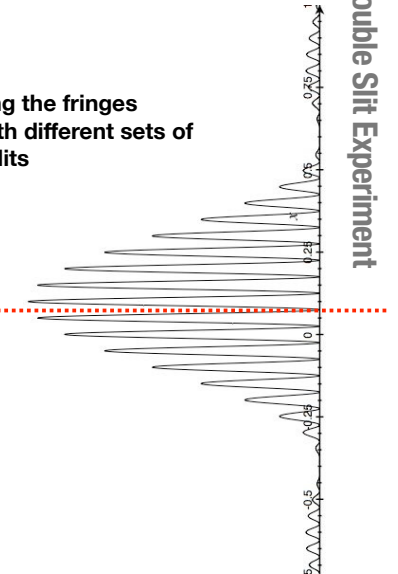
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Observing the fringes taken with different sets of double slits



candidate

candidate



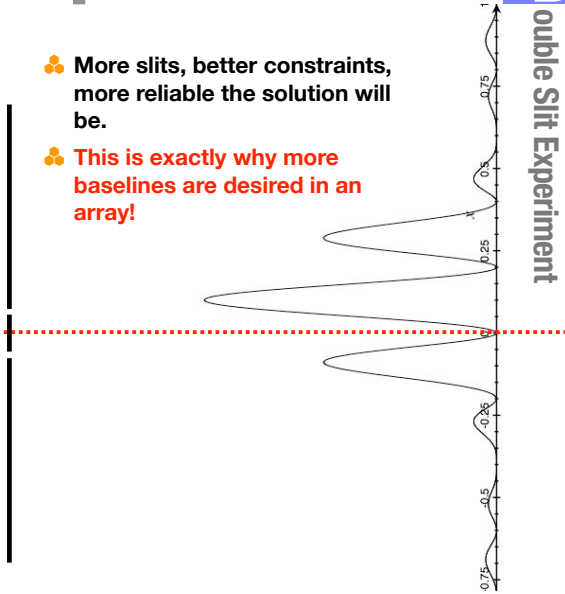
Double Slit Experiment

Double-slit Experiment

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- More slits, better constraints, more reliable the solution will be.
- This is exactly why more baselines are desired in an array!

★ Got you!



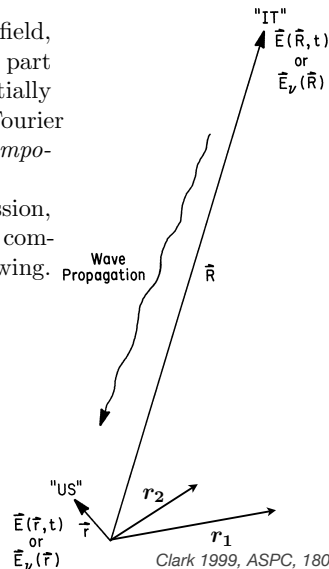
Observed Electric Field

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Consider a finite time interval of a varying field, whose magnitude may be expressed as the real part of the sum of the Fourier series with exponentially time-varying functions. The coefficients of this Fourier series, $E_\nu(\mathbf{R})$, are the *quasi-monochromatic components* of the electric field, $\mathbf{E}(\mathbf{R}, t)$. To avoid unnecessary complications of the discussion, let's consider only a single quasi-monochromatic component and introduce five assumptions as following.

Scalar field assumption. Ignore the fact that EM wave is a vector phenomenon, and treat it as if it were simply a scalar field.

Projection on a celestial sphere. Project all the emitting phenomena on a celestial sphere without describing the structure of the emitting regions in the their dimension.



Clark 1999, ASPC, 180, 1

Spatial Coherence Function I

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Propagation through the vacuum. The space within the celestial sphere is empty, and Huygens' Principle can be applied

$$E_\nu(\mathbf{r}) = \int E_\nu(\mathbf{R}) \frac{e^{2\pi i \nu |\mathbf{R}-\mathbf{r}|/c}}{|\mathbf{R}-\mathbf{r}|} dS,$$

where dS is the element of surface area on the celestial sphere. The correlation of the field at points \mathbf{r}_1 and \mathbf{r}_2 is defined as

$$V_\nu(\mathbf{r}_1, \mathbf{r}_2) \equiv \langle E_\nu(\mathbf{r}_1) E_\nu^*(\mathbf{r}_2) \rangle = \left\langle \int \int E_\nu(\mathbf{R}_1) E_\nu^*(\mathbf{R}_2) \frac{e^{2\pi i \nu |\mathbf{R}_1-\mathbf{r}_1|/c}}{|\mathbf{R}_1-\mathbf{r}_1|} \frac{e^{2\pi i \nu |\mathbf{R}_2-\mathbf{r}_2|/c}}{|\mathbf{R}_2-\mathbf{r}_2|} dS_1 dS_2 \right\rangle$$

Spatially incoherent emission. Assuming that the radiation from sources is not spatially coherent, i.e. $\langle E_\nu(\mathbf{R}_1) E_\nu^*(\mathbf{R}_2) \rangle = 0$ for $\mathbf{R}_1 \neq \mathbf{R}_2$, we obtain

$$V_\nu(\mathbf{r}_1, \mathbf{r}_2) = \int \langle |E_\nu(\mathbf{R})|^2 \rangle \frac{e^{2\pi i \nu |\mathbf{R}-\mathbf{r}_1|/c}}{|\mathbf{R}-\mathbf{r}_1|} \frac{e^{2\pi i \nu |\mathbf{R}-\mathbf{r}_2|/c}}{|\mathbf{R}-\mathbf{r}_2|} dS.$$

Spatial Coherence Function II

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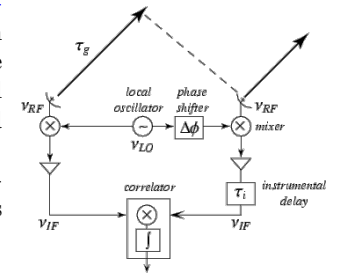
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Substituting \mathbf{s} for the unit vector $\mathbf{R}/|\mathbf{R}|$, $I_\nu(\mathbf{s})$ for the observed intensity $c \langle |E_\nu(\mathbf{s})|^2 \rangle / 4\pi$, $d\Omega$ for the solid angle $dS/|\mathbf{R}|^2$, and neglecting all terms with $|\mathbf{r}/\mathbf{R}|$, we obtain the spatial coherence function

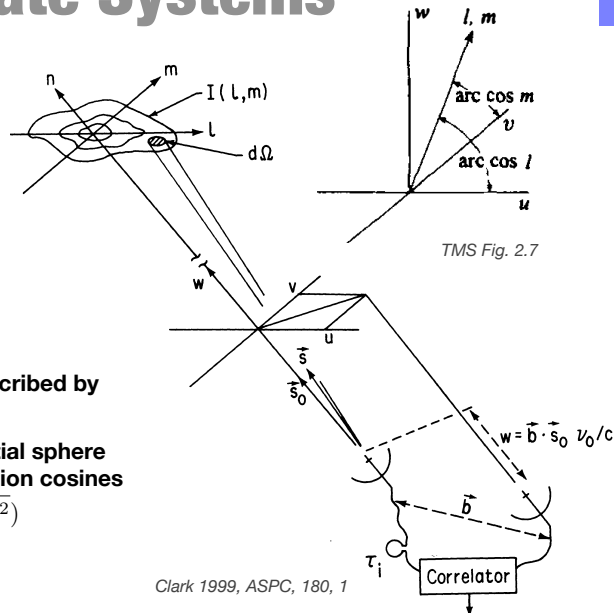
$$V_\nu(\mathbf{r}_1, \mathbf{r}_2) \simeq \int I_\nu(\mathbf{s}) e^{-2\pi i \nu \mathbf{s} \cdot (\mathbf{r}_1 - \mathbf{r}_2) / c} d\Omega.$$

An interferometer is a device for measuring the spatial coherence function. The intensity distribution of the radiation as a function of direction \mathbf{s} can be deduced in certain cases by measuring the spatial coherence function V as a function of $\mathbf{r}_1 - \mathbf{r}_2$ and performing the inversion.

Further simplification involves our fifth and final assumption, which can be argued with two special cases of great interest.



Coordinate Systems



- Measurements described by $\lambda(u, v, w)$
- Radiation on celestial sphere described by direction cosines $(l, m, \sqrt{1-l^2-m^2})$

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erture Synthesis

Spatial Coherence Function IV

Coplanar Arrays. The first special case consider making all the measurements in a plane, i.e. $\mathbf{r}_1 - \mathbf{r}_2 = \lambda(u, v, w = 0)$. The spatial coherence function will take the form

$$V_\nu(u, v, w = 0) = \iint I_\nu(l, m) \frac{e^{-2\pi i(ul+vm)}}{\sqrt{1-l^2-m^2}} dl dm.$$

Sources in a small patch of sky. The second special case consider all the radiation of interest comes from only a small portion of the celestial sphere, i.e. $\mathbf{s} = \mathbf{s}_0 + \boldsymbol{\sigma}$ with $\mathbf{s}_0 \cdot \boldsymbol{\sigma} = 0$. In other words, $|l|$ and $|m|$ are small that $(\sqrt{1-l^2-m^2}-1)w \simeq 0$ and the spatial coherence function becomes

$$V_\nu(u, v) = \iint I_\nu(l, m) e^{-2\pi i(ul+vm)} dl dm,$$

where $V_\nu(u, v)$ is the coherence function relative to the **phase tracking center**, \mathbf{s}_0 .

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Spatial Coherence Function III

Given the direction cosines, we choose $\mathbf{s} = (l, m, \sqrt{1-l^2-m^2})$ and $\mathbf{s}_0 = (0, 0, 1)$ so that

$$\frac{\nu \mathbf{s} \cdot (\mathbf{r}_1 - \mathbf{r}_2)}{c} = ul + vm + wn,$$

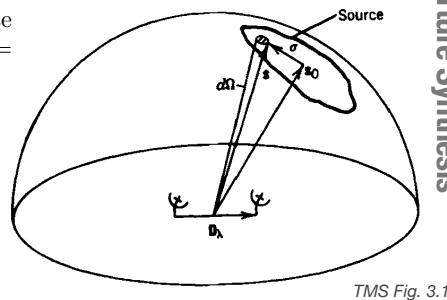
$$\frac{\nu \mathbf{s}_0 \cdot (\mathbf{r}_1 - \mathbf{r}_2)}{c} = w$$

$$d\Omega = \frac{dl dm}{n} = \frac{dl dm}{\sqrt{1-l^2-m^2}}.$$

Substituting the above relations, we find the spatial coherence function to be

$$V_\nu(u, v, w) = \iint I(l, m) e^{-2\pi i[ul+vm+w(\sqrt{1-l^2-m^2}-1)]} \frac{dl dm}{\sqrt{1-l^2-m^2}},$$

where the integral is taken to be zero for $l^2 + m^2 \geq 1$.



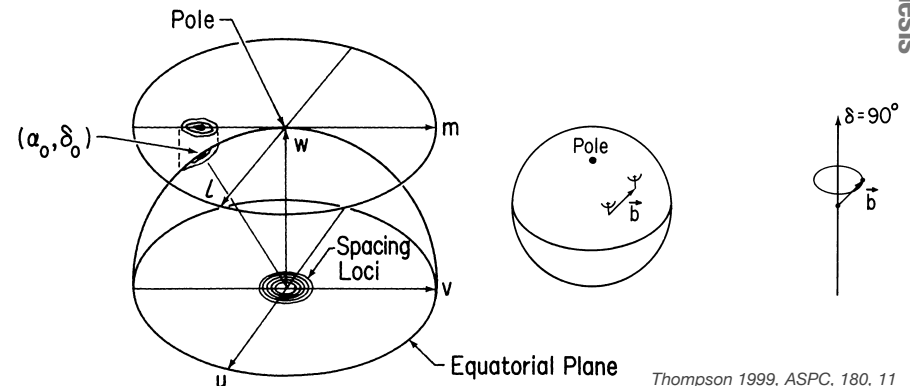
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Coplanar Arrays

- Coplanar array can be formed by placing all baselines along an East-West line, which zeros the components of the baseline vector parallel to the Earth's axis
- Distortion occurs at low elevation



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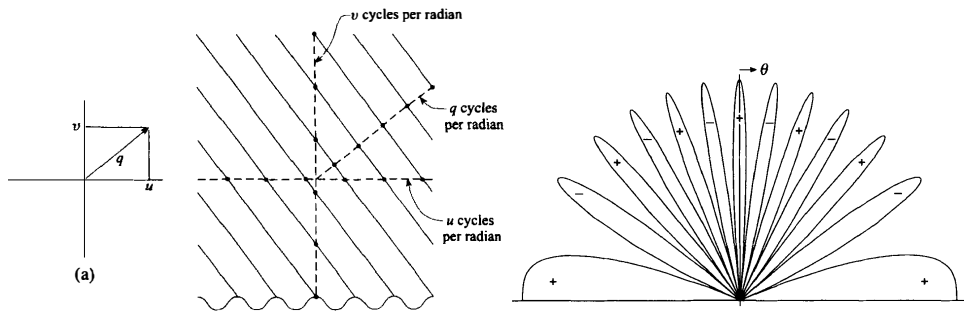
Response of Interferometers

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The complex visibility of the source is defined as

$$V_\nu(u, v) = \iint I_\nu(l, m) e^{-2\pi i(ul+vm)} dl dm$$

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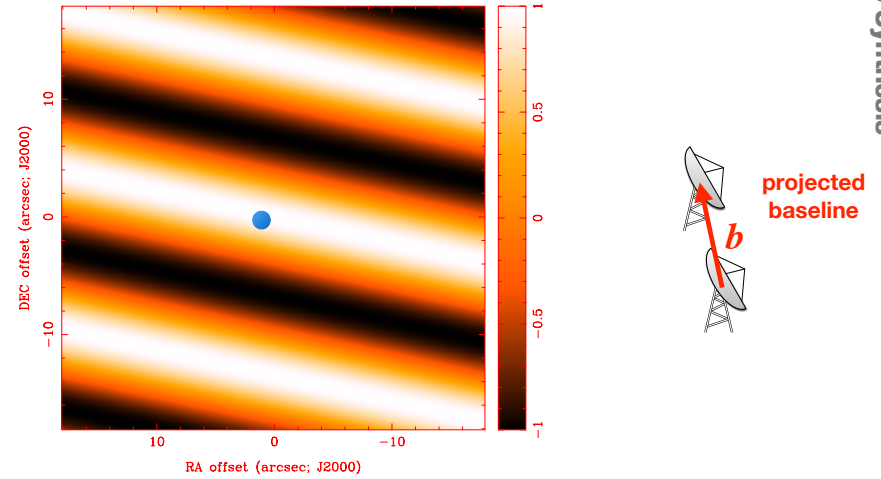


Visibility

A

$$V_\nu(u, v) = \iint I_\nu(l, m) e^{-2\pi i(ul+vm)} dl dm$$

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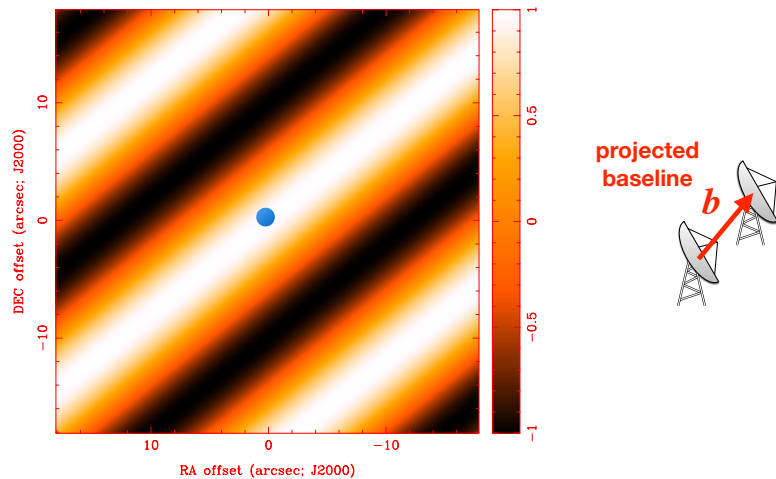


Visibility

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$$V_\nu(u, v) = \iint I_\nu(l, m) e^{-2\pi i(ul+vm)} dl dm$$

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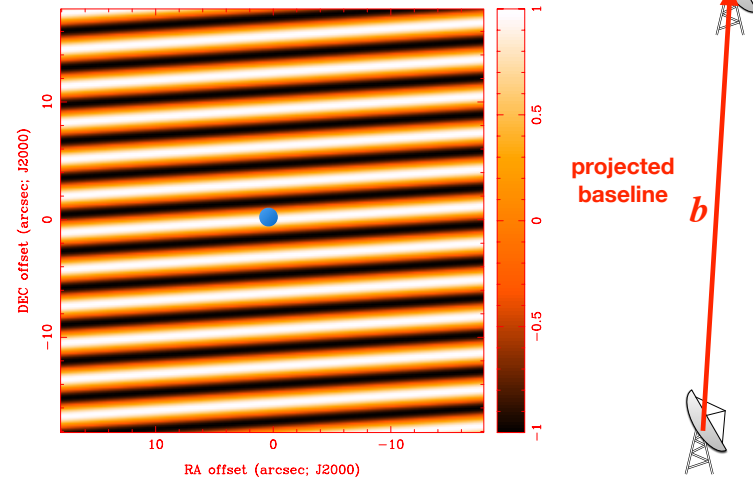


Visibility

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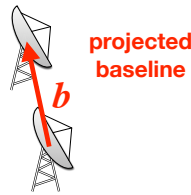
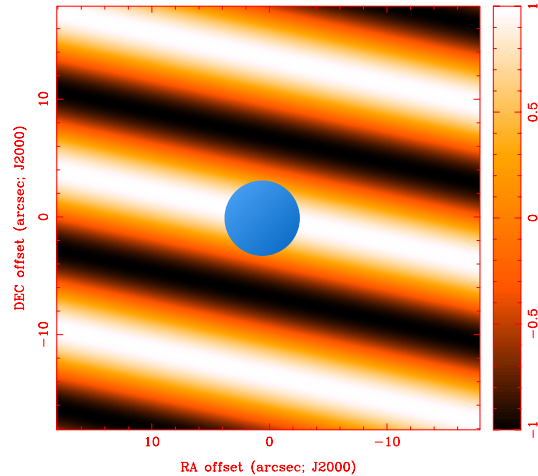
$$V_\nu(u, v) = \iint I_\nu(l, m) e^{-2\pi i(ul+vm)} dl dm$$

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Visibility

$$V_\nu(u, v) = \iint I_\nu(l, m) e^{-2\pi i(ul+vm)} dl dm$$



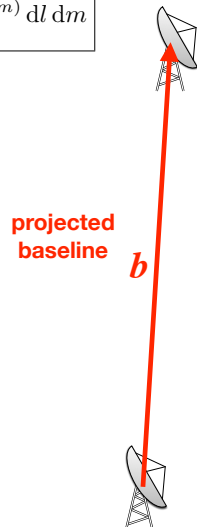
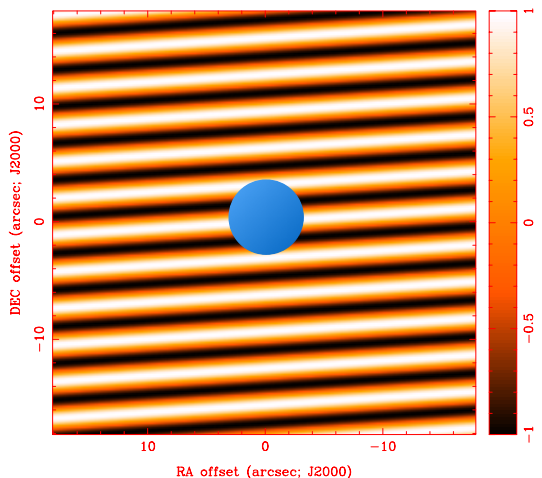
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Visibility - Resolved Out

$$V_\nu(u, v) = \iint I_\nu(l, m) e^{-2\pi i(ul+vm)} dl dm$$



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Response of Interferometer I

The **correlator** is a voltage multiplier followed by a time averaging (integrating) circuit. Consider the received signals by quasi-monochromatic Fourier components of the form

$$V_1(t) = v_1 \cos 2\pi\nu(t - \tau_g)$$

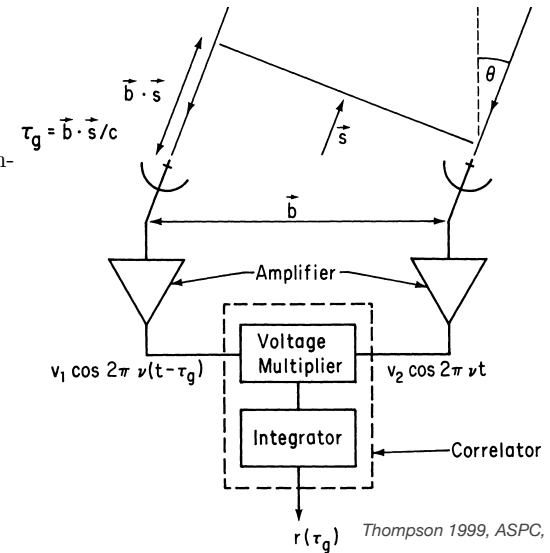
$$V_2(t) = v_2 \cos 2\pi\nu t.$$

The output from the correlator is proportional to

$$r(\tau_g) = \langle V_1(t)V_2(t) \rangle$$

$$= v_1 v_2 \cos 2\pi\nu\tau_g,$$

where τ_g varies slowly with time as the Earth rotates.



Thompson 1999, ASPC, 180, 11

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erture Synthesis

Response of Interferometer II

The signal power received in bandwidth $\Delta\nu$ from the source element $d\Omega$ is $A(\mathbf{s})I(\mathbf{s})\Delta\nu d\Omega$, where $A(\mathbf{s})$ is the effective collecting area. Since the terms $v_1 v_2$ represents the fringe amplitude and is proportional to the received power, we can represent the correlator output by

$$dr = A(\mathbf{s})I(\mathbf{s})\Delta\nu d\Omega \cos 2\pi\nu\tau_g$$

$$= \Delta\nu \int A(\mathbf{s})I(\mathbf{s}) \cos \frac{2\pi\nu \mathbf{b} \cdot \mathbf{s}}{c} d\Omega.$$

In the case where the radiation comes from a small patch of sky, we rewrite $\mathbf{s} = \mathbf{s}_0 + \boldsymbol{\sigma}$ and obtain

$$r = \Delta\nu \cos \left(\frac{2\pi\nu \mathbf{b} \cdot \mathbf{s}_0}{c} \right) \int A(\boldsymbol{\sigma})I(\boldsymbol{\sigma}) \cos \left(\frac{2\pi\nu \mathbf{b} \cdot \boldsymbol{\sigma}}{c} \right) d\Omega$$

$$- \Delta\nu \sin \left(\frac{2\pi\nu \mathbf{b} \cdot \mathbf{s}_0}{c} \right) \int A(\boldsymbol{\sigma})I(\boldsymbol{\sigma}) \sin \left(\frac{2\pi\nu \mathbf{b} \cdot \boldsymbol{\sigma}}{c} \right) d\Omega$$

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Response of Interferometer III

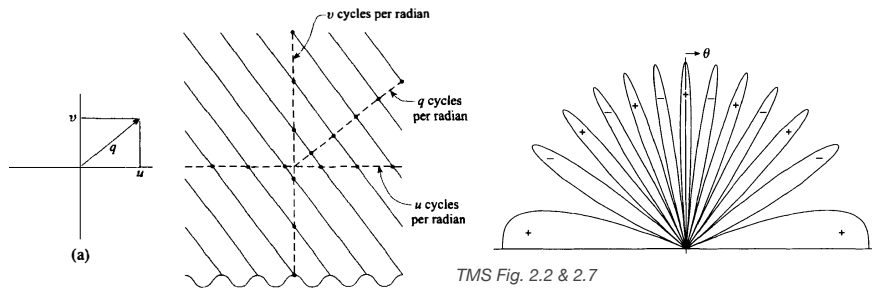
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The complex visibility of the source is defined as

$$V \equiv |V|e^{i\phi_V} = \int \mathcal{A}(\boldsymbol{\sigma}) I(\boldsymbol{\sigma}) e^{-2\pi i \nu \mathbf{b} \cdot \boldsymbol{\sigma} / c} d\Omega.$$

Substituting the complex visibility, we find the response

$$r = A_0 \Delta \nu |V| \cos \left(\frac{2\pi \nu \mathbf{b} \cdot \mathbf{s}_0}{c} - \phi_V \right).$$



TMS Fig. 2.2 & 2.7

Effect of Discrete Sampling

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Given the above relationship between $V_\nu(u, v)$ and $I_\nu(l, m)$, it is obvious that the direct inversion reads

$$I_\nu(l, m) = \iint V_\nu(u, v) e^{2\pi i (ul+vm)} du dv.$$

In practice, V_ν is not known everywhere but is sampled at particular places on the $u-v$ plane described by a **sampling function**, $S(u, v)$, that $S(u, v) = 0$ where no data have been taken. One can compute

$$I_\nu^D(l, m) = \iint V_\nu(u, v) S(u, v) e^{2\pi i (ul+vm)} du dv,$$

where $I_\nu^D(l, m)$ is referred to as the **dirty image**; its relation to the ideal intensity distribution is

$$I_\nu^D = I_\nu \otimes B,$$

where $B(l, m)$ is the so-called **synthesized beam** or point spread function

$$B(l, m) = \iint S(u, v) e^{2\pi i (ul+vm)} du dv.$$

Effect of Primary Beam

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In practice, the interferometer elements are not point probes which sense the voltage at that point, but are elements of finite size and directional sensitivity. The normalized reception pattern of each element, i.e. the **primary beam** needs to be included

$$V_\nu(u, v) = \iint \mathcal{A}_\nu(l, m) I_\nu(l, m) e^{-2\pi i (ul+vm)} dl dm,$$

where $\mathcal{A}_\nu(l, m) = A_\nu(l, m)/A_{\nu,0}$.

The calibration with the element directional sensitivity \mathcal{A}_ν should be postponed to the final step of deriving the sky intensity distribution and it should simply divide the derived intensities. Such division is often referred to as **primary beam correction** and will, however, not only produce a better estimate of the actual intensities in this direction, but will also increase the errors in directions far from the phase tracking center.

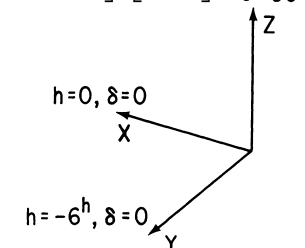
Projection of Baselines I

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With multi-element arrays, it is convenient to specify the antenna positions in a Cartesian coordinate system. For example, a system with X the direction of the meridian at the celestial equator, Y the East, and Z toward the North celestial pole. Let L_X , L_Y , and L_Z the corresponding coordinate differences for two antennas, the baseline components (u, v, w) are given by

$$\begin{bmatrix} u \\ v \\ w \end{bmatrix} = \frac{1}{\lambda} \begin{bmatrix} \sin H_0 & \cos H_0 & 0 \\ -\sin \delta_0 \cos H_0 & \sin \delta_0 \sin H_0 & \cos \delta_0 \\ \cos \delta_0 \cos H_0 & -\cos \delta_0 \sin H_0 & \sin \delta_0 \end{bmatrix} \begin{bmatrix} L_X \\ L_Y \\ L_Z \end{bmatrix}, \quad \delta = 90^\circ$$

where H_0 and δ_0 are the hour angle and declination of the phase reference position. The elements in the transformation matrix are the direction cosines of the (u, v, w) axes relative to (X, Y, Z) axes.

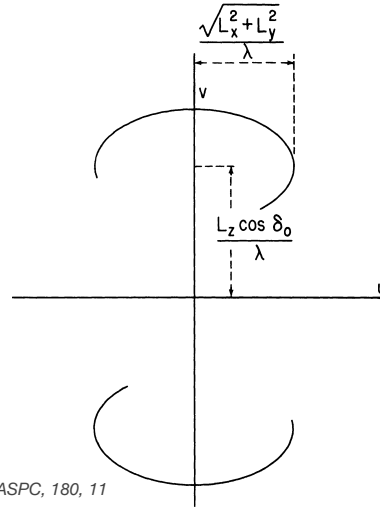


Projection of Baselines II

Eliminating H_0 from the expressions for u and v , we can obtain the equation of an ellipse in the (u, v) plane:

$$u^2 + \left(\frac{v - (L_z/\lambda) \cos \delta_0}{\sin \delta_0} \right)^2 = \frac{L_X^2 + L_Y^2}{\lambda^2}$$

The ellipse is simply the projection onto the (u, v) plane of the circular locus traced out by the tip of the baseline vector. Since $I(l, m)$ is real, $V(-u, -v) = V^*(u, v)$. For an array of antennas, the ensemble of elliptical loci is the **sampling function**, $S(u, v)$.



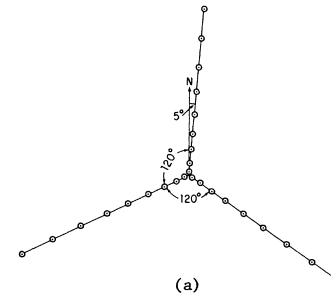
Thompson 1999, ASPC, 180, 11

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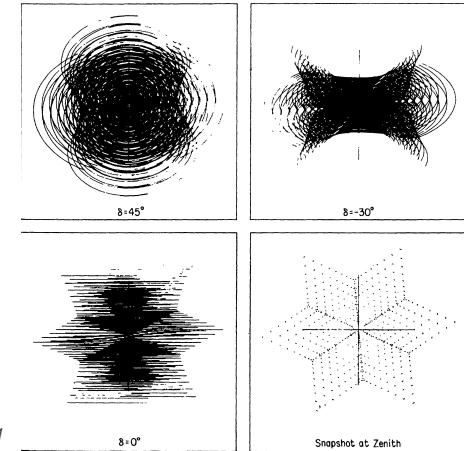
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VLA u-v Tracks



Thompson 1999, ASPC, 180, 11

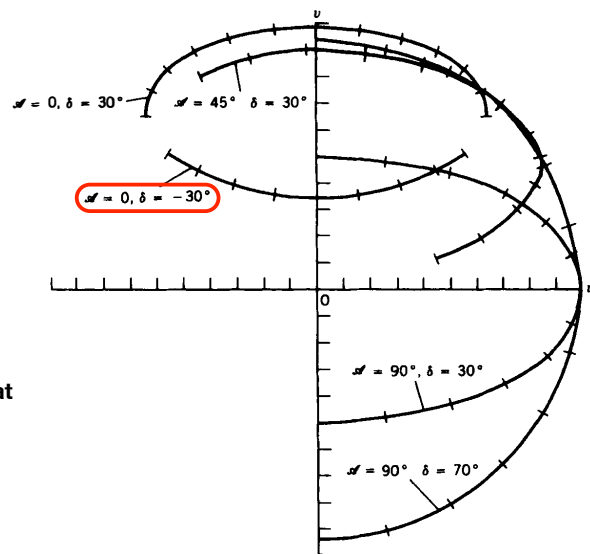


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Projection of Baselines III



• Loci for an array at latitude +40°

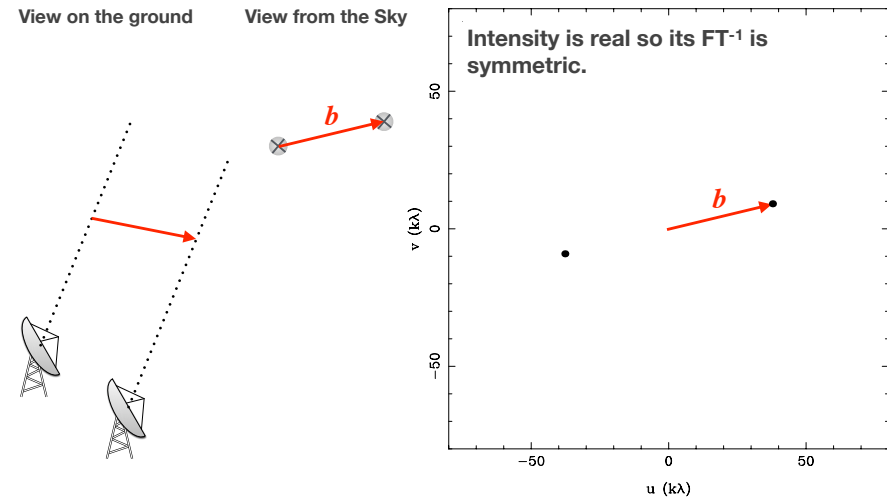
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The u-v Plane

2 antennas, 1 sample



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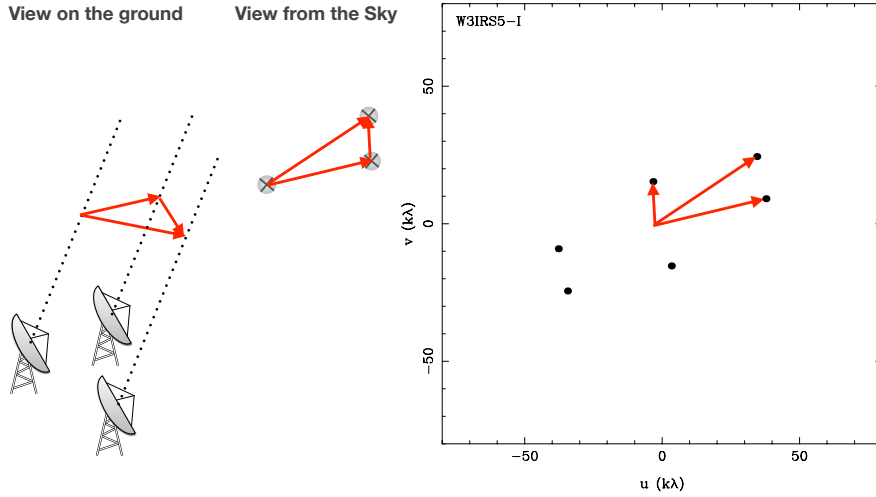
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The u-v Plane

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3 antennas, 1 sample



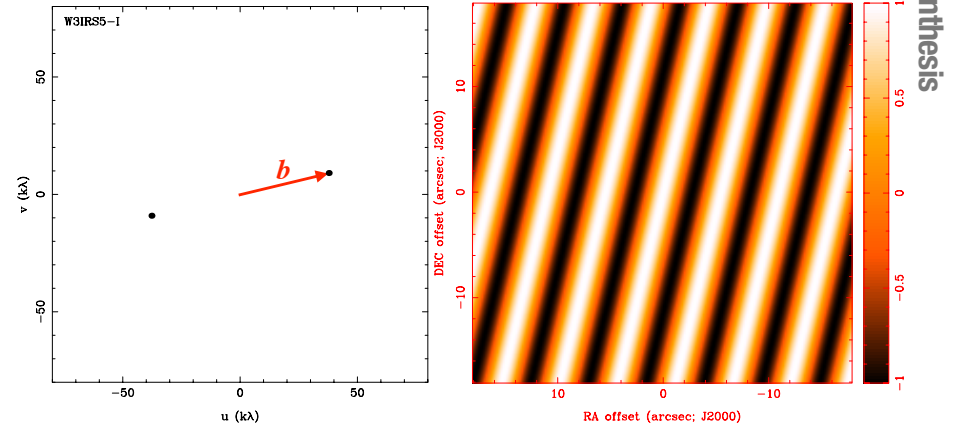
Aperture Synthesis

Aperture Synthesis

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2 antennas, 1 sample



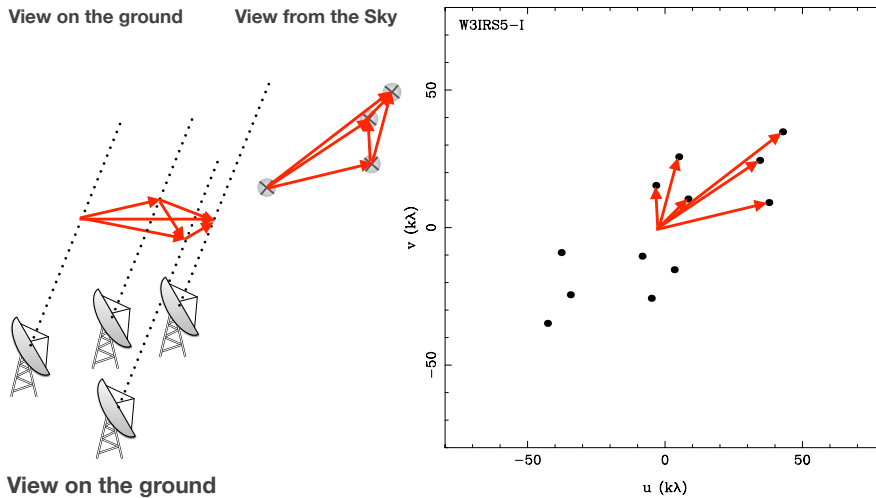
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The u-v Plane

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4 antennas, 1 sample



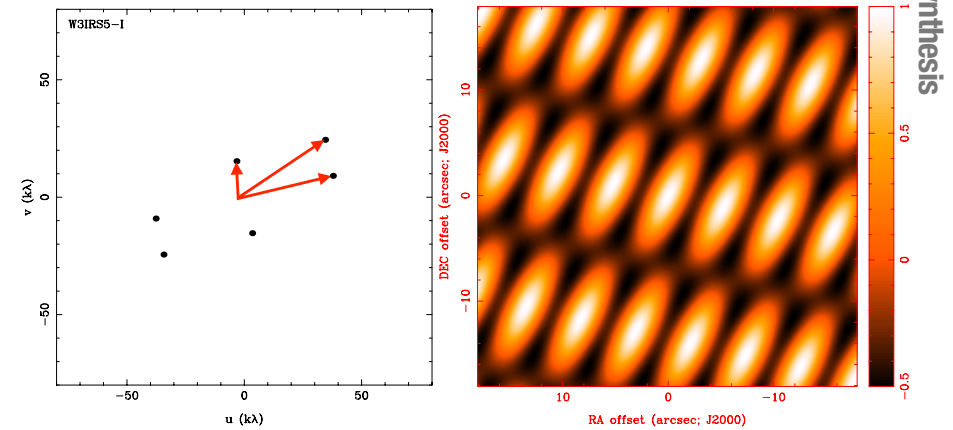
Aperture Synthesis

Aperture Synthesis

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3 antennas, 1 sample



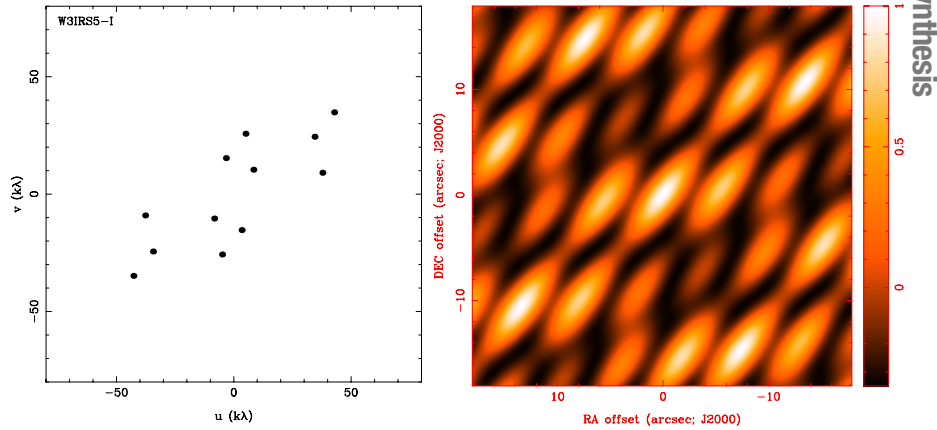
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Aperture Synthesis

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4 antennas, 1 sample

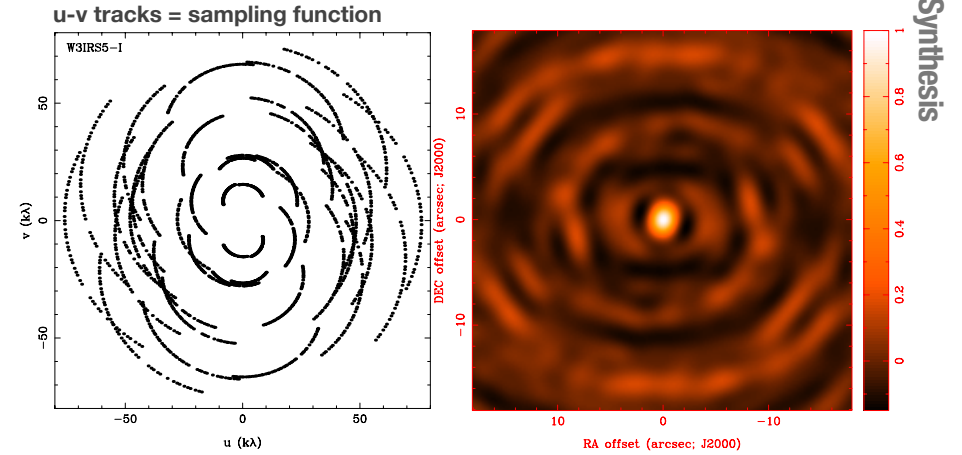


Aperture Synthesis

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7 antennas, full track

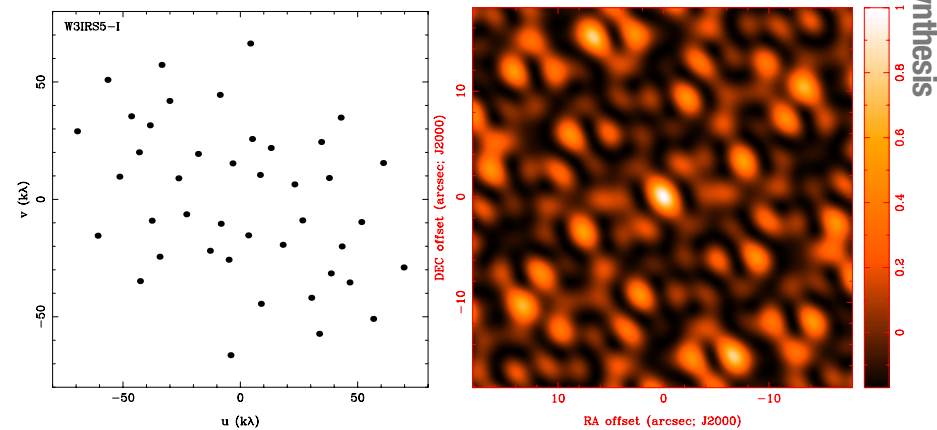


Aperture Synthesis

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7 antennas, 1 sample



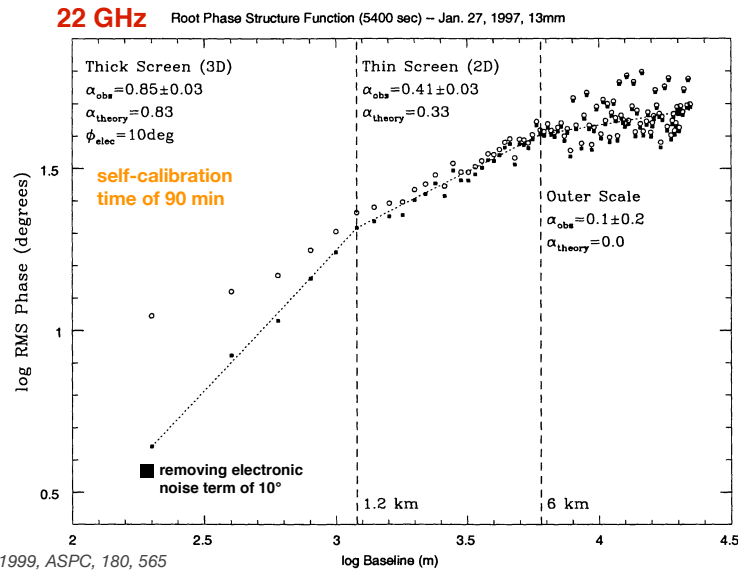
Observation Strategy with Interferometers

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Aperture Synthesis

Tropospheric Phase Fluctuation



Atmospheric Effects

Gain Calibration I

Since the visibility is sampled at discrete times for each antenna pair, the array synthesis formulation is often written as

$$V_{ij}(t) = \iint \mathcal{A}_\nu(l, m) I_\nu(l, m) e^{-2\pi i [u_{ij}(t)l + v_{ij}(t)m]} dl dm.$$

The observed visibilities, $\tilde{V}_{ij}(t)$, can be related to the true visibilities, V_{ij} through

$$\tilde{V}_{ij}(t) = G_{ij}(t)V_{ij}(t) + \varepsilon_{ij}(t) + n_{ij}(t),$$

where

G_{ij} = baseline-based complex gain

ε_{ij} = baseline-based complex offset

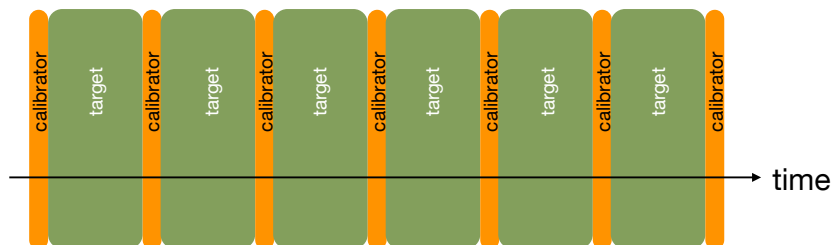
n_{ij} = stochastic complex noise

The complex offset, ε_{ij} , and complex noise, n_{ij} , are merely the complex resultants of the offsets and noises of two independent correlators and should not lower the coherence perceptibly.

Aperture Synthesis

Basic Calibration Types

- Bandpass calibration: correct frequency response by observing a bright source of featureless spectrum
- Flux calibration: correct visibility amplitudes by observing a source of known flux density
- Gain calibration: correct temporal phase fluctuation by repeatedly observing a calibrator of known structures to track what the troposphere is doing



Aperture Synthesis

Gain Calibration II

The baseline-based complex gain, G_{ij} can often be approximated by the product of the two associated **antenna-based complex gains**, g_i and g_j ,

$$G_{ij}(t) = g_i(t)g_j^*(t) = a_i(t)a_j(t) e^{i[\phi_i(t) - \phi_j(t)]},$$

where $a_i(t)$ is the **gain amplitude** correction and $\phi_i(t)$ the **gain phase** correction.

In practice, the antenna-based gains are not only a function of time but also frequency

$$g_i(\nu, t) = g_i(t)g_i(\nu),$$

where $g_i(\nu)$ is the so-called passband gains, which describes the (assumed non-varying) response of the system across frequency bands. The process of solving for $g_i(\nu)$ is often referred to as the **bandpass calibration**.

Aperture Synthesis

Software Packages

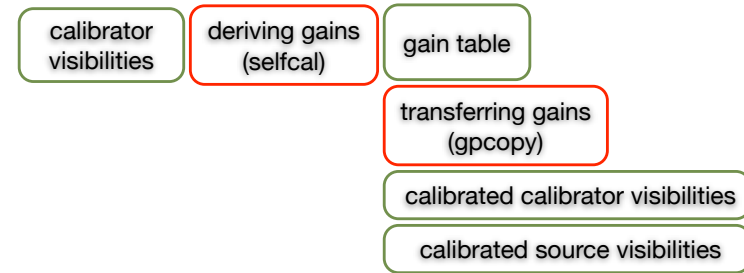
- 🔥 All are free and available online
- 🔥 **MIRIAD = Multichannel Image Reconstruction, Image Analysis, and Display**
 - 🔥 Developed by radio astronomers associated with ATFA and BIMA
 - 🔥 Mainly used for BIMA, ATCA, CARMA, SMA
 - 🔥 **Versions**
 - 🔥 MIRIAD3: BIMA, ATCA
 - 🔥 MIRIAD4: SMA, CARMA
- 🔥 **AIPS**
 - 🔥 Developed by NRAO mainly for VLA and single dishes, e.g. KP 12m
- 🔥 **Gildas**
 - 🔥 Developed by ESO mainly for PdBI and IRAM 30m
- 🔥 **CASA**
 - 🔥 Developed by NRAO mainly for JVLA and ALMA

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Visibility Calibration



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From Visibility to Images

Observed quantities:

Visibilities $V(u, v)S(u, v) = \int \int \mathcal{A}(l, m) I(l, m) e^{-2\pi i(ul+vm)} dl dm$

Sampling function $S(u, v) = \sum_{k=1}^N \delta(u - u_k, v - v_k)$

Generating images from visibilities:

Synthesized beam $B(l, m) = \int \int S(u, v) e^{2\pi i(ul+vm)} du dv$

Dirty map $I^D(l, m) = [\mathcal{A}(l, m) I(l, m)] \otimes B(l, m)$
 $= \int \int V(u, v) S(u, v) e^{2\pi i(ul+vm)} du dv$

Weighted visibilities $V^W(u, v) = \sum_{k=1}^N R_k T_k D_k V(u, v)$

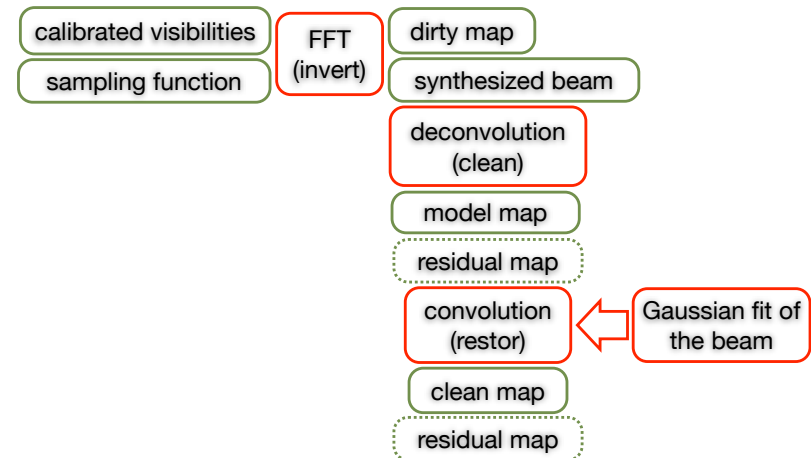
where R_k , T_k , and D_k are weights assigned to the visibilities indicating their reliability, the tapering, and the density weighting.

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“Clean” Images



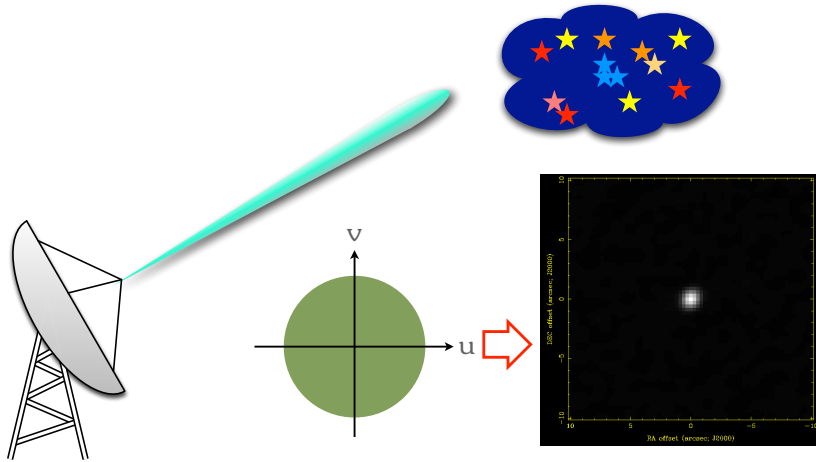
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Why Restoring a Beam?

Single-dish comes with a more or less ideal beam



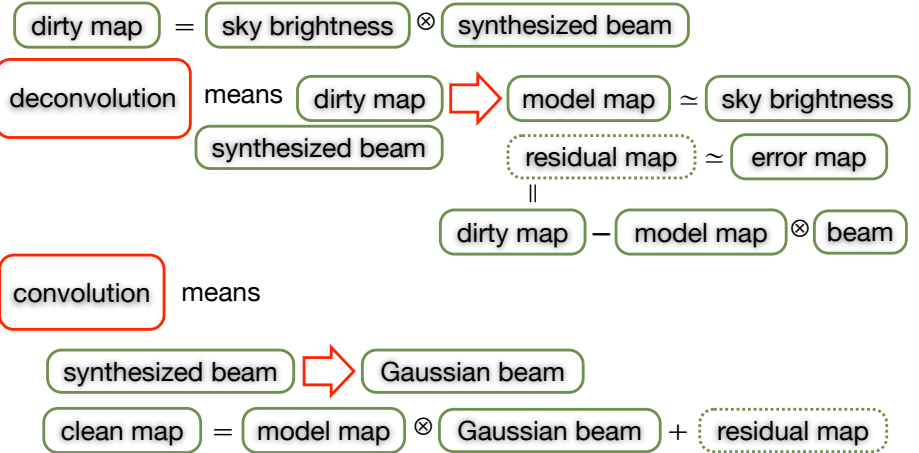
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Replacing Synthesized Beam

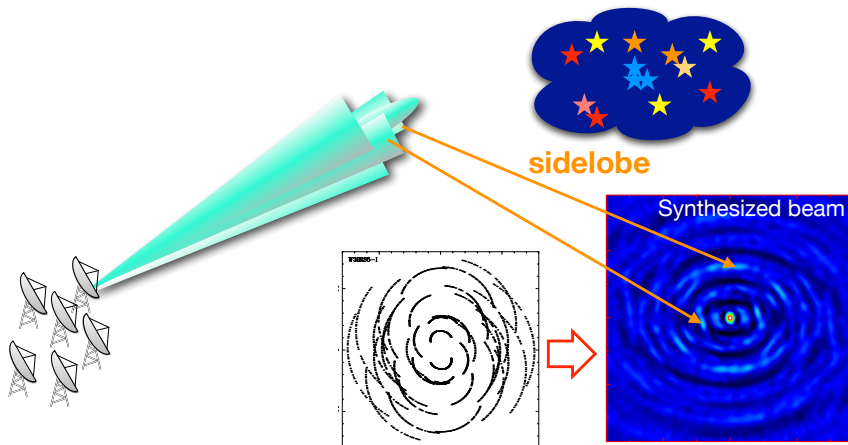
CLEAN Task in CASA



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Why Restoring a Beam?

Incomplete sampling with an array leads to a non-ideal beam with sidelobes

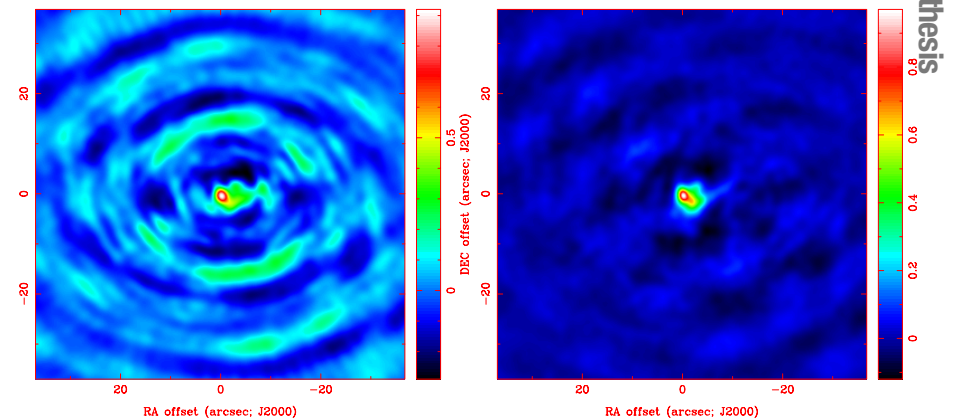


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Dirty Map vs Clean Map



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